

Dynamic system modeling for control and diagnosis

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Energy system modeling,
Fundamentals of thermodynamics and the
model equations



Contents

- Introduction to thermodynamics
 - System and environment
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 - Description of the system, statevariables
 - Extensive and intensive quantities
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 - Heated solid pipe
 - Water pipe
 - Steam generator
 - Steam collector



Introduction to thermodynamics (thermostatistics)

- Concerns heat, energy, work, interaction between bodies, cycles
- Describes the *macroscopic* behaviour of the processes
- Phenomenological description
- Very common laws (energy conservation, direction of spontaneous processes) – widely reusable (in economics, black holes ...)
- Macroscopic variables:
 - Temperature, pressure
 - Density, specific heat,
 - Inner energy, enthalpy,
 - Entropy
 - etc



Introduction

- Thermodynamic fields:
 - Engines, cycles (Carnot cycle), efficiency
 - Phase transitions
 - Chemical reactions
 - Transport (fluids, heat, mass, energy...)

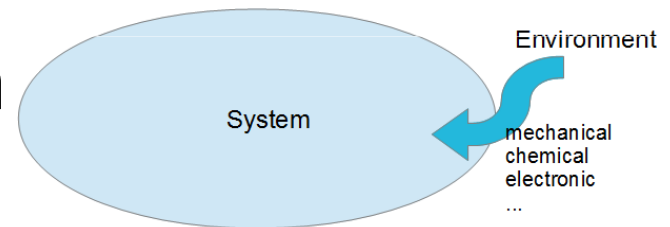
Statevariables



ISOLATED SYSTEM DESCRIPTION

System and environment

- *System and environment*
 - We have to define them
 - Usually the system does not change the state of the environment
- *Macroscopic description*
 - Much larger than an atom
 - Not sensible by senses
- *Physical state description*
 - Measurable physical quantities
 - 2 groups: *extensive* and *intensive* quantities



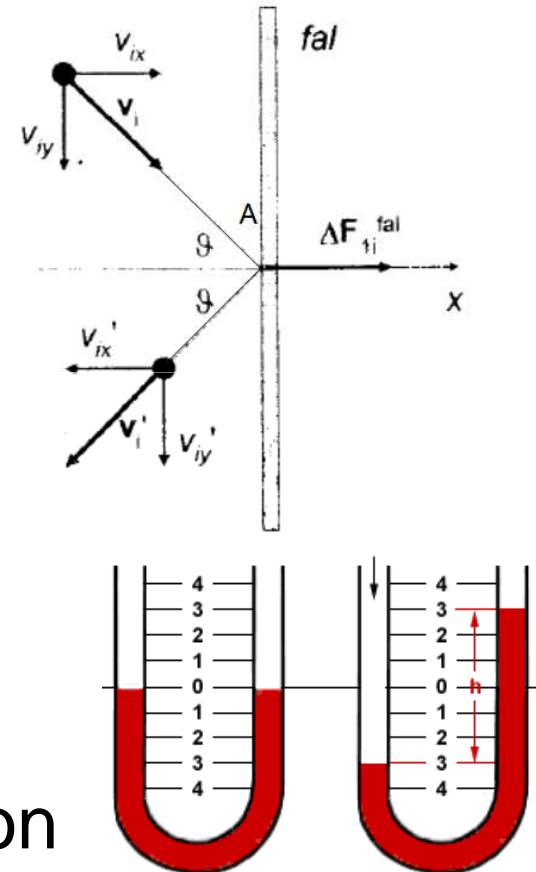


System and equilibrium

- System in an environment
 - Usually there are interaction between them
- Isolated system:
 - No interaction between the system and its environment
 - System will be in *equilibrium*:
 - The state does not change any more
 - States (állapotjellemzők):
 - Describes the system in equilibrium
 - Any two equilibrium can be distinguished by the state variables

Description of the system - state variables

- Pressure:
 - Pa (SI), $1 \text{ Pa} = 1 \text{ N/m}^2$
 - 1 atm, 1 bar, 10^5 Pa
 - Collisions of molecules and the wall
 - Absolute and overpressure
 - The pressure is independent of the direction



Statevariables

- Temperature
 - Measurement units: °C (Celsius), K (Kelvin)
 - Absolute zero (0 K = -273,15°C)
 - Measurement is complicated:
 - Needs a zero point and a linear scale
 - The thermometer has heat capacity
 - The temperature change has different effects, which can be used to measure
 - Heat expansion coefficient: $\frac{1}{V} \frac{\partial V}{\partial T} = \beta$

Statevariables

- Amount of substance (anyagmennyiség mólszám)
 - Measurement unit is: mol
 - 1 mol is the number of atoms in 12g C-12 isotope
 - 1 mol = 6.022×10^{23} molecules or atom (Avogadro's number)
 - Number of atoms (N)
- Further properties:
 - Density and specific volume $\rho = \frac{1}{\nu}$
 - Specific heat capacity

Extensive and intensive quantities

- Extensives:

- Additivity
- If you divide the system into two half, the quantity will be the half in each
- Volume, energy, mass, number of molecules etc.
- Locally cannot be defined

$$\begin{array}{l} V_1, m_1, E_1, n_1 \quad V_2, m_2, E_2, n_2 \\ \\ V = V_1 + V_2 \\ M = M_1 + M_2 \\ E = E_1 + E_2 \\ N = n_1 + n_2 \end{array}$$

- Intensives:

- Non-additive
- Locally can be defined
- Inhomogeneity cause flows
- Pressure, density, temperature ...

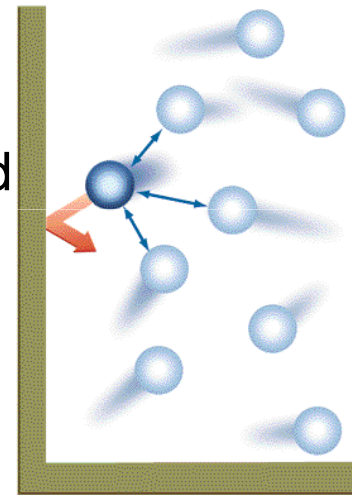
$$\begin{array}{l} N_1, T_1 \quad N_2, T_2 \\ \\ T = \frac{N_1 T_1 + N_2 T_2}{N_1 + N_2} \end{array}$$



IDEAL AND REAL GAS LAW'S

Basic system – ideal gas

- Ideal gas properties:
 - Gas molecules are *small balls*, the diameter of which can be neglected comparing to the *free path* (average distance between two collisions)
 - The only interaction between the molecules and between the molecules and vessel's wall is the elastic collision.
 - The movement direction of the molecules are random.
- Mass (m) / amount of substance (n), volume (V), pressure (p), temperature (T) describes the gas state.



Ideal gas law

- Boyle-Mariotte law:

- $p_1 V_1 = p_2 V_2 = \text{const.}$ if the temperature is const.

- Gay-Lussac law:

- I.: $\frac{V_1}{T_1} = \frac{V_2}{T_2} = \text{const.}$ if p is constant
- II.: $\frac{p_1}{T_1} = \frac{p_2}{T_2} = \text{const.}$ if V is constant

- Avogadro's law:

- $\frac{n_1}{V_1} = \frac{n_2}{V_2} = \text{const.}$ if p and T const.

- **Combined gas law:**

- $pV = nRT$, where the universal gas constant $R=8.31 \text{ J/mol/K}$

Real gas laws

- Van-der-Waals state equation:
 - In real gases there exist an attraction force between the particles which results higher pressure than in the ideal gas:

$$p + \frac{n^2 a}{V^2} = p_{id}$$

- In real gases the volume of the particles cannot be neglected, so there is smaller space in the vessel, than in the ideal case:

$$V - nb = V_{id}$$

- Substitute into the ideal gas law:

$$\left(p + \frac{n^2 a}{V^2}\right)(V - nb) = nRT$$



Real gas laws

- Van der Waals
 - describes *better* the gases than the ideal gas law, but there are dozens of state-equations for various gases under different conditions
- Steam tables
 - contains the properties of water and steam in different regions
 - This are the most accurate source of information



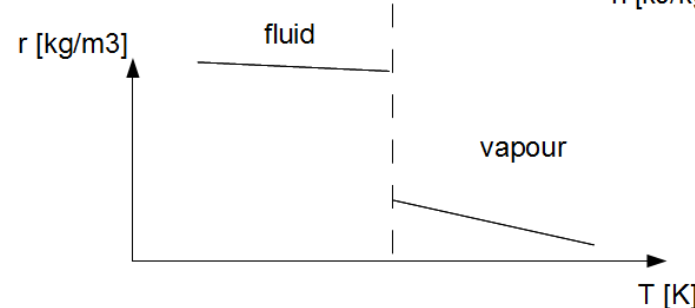
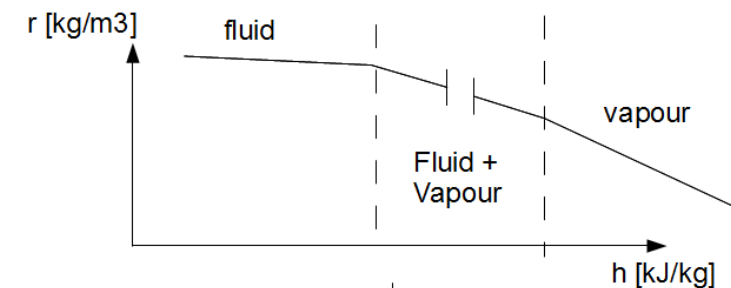
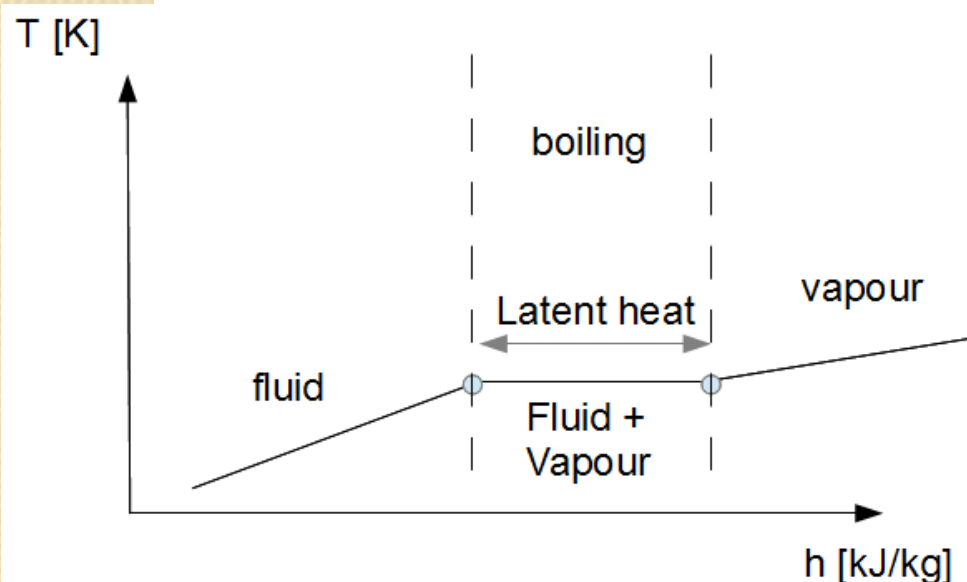
THE WATER

The water and steam

- Most important media
 - Most frequently used material in the industries
- Accurate properties in steam tables
- 3 free parameter:
 - Pressure, temperature, volume
 - Pressure and enthalpy, volume
 - Etc.
- 2 parameter + saturated condition
 - $p_{\text{sat}} = p_{\text{sat}}(T_{\text{sat}})$

How to choose the state variables?

- Usual choice of intensive state variables:
 - In case of phase transition:
 - Pressure and enthalpy
 - Temperature is constant during the transition
 - In case there is no phase-transition
 - Pressure and temperature



Firefox | W Intensive and extensive properties - ... | W Hőátviteli együttható - Wikipédia | Gmail - Beérkező levelek (1) - gabor.a... | Steam Tables Calculator

www.steamtablesonline.com/steam97web.aspx

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1. General Properties | 2. Saturation Properties | 3. Steam Turbine | 4. Flash Evaporator | 5. T-S Diagram | 6. H-S Diagram | 7. H-S Diagram (vapor) | 8. Gas Tables | Setup Pane

Input Data

Select function: 1. function (p, t)

1. Pressure (absolute): 50 bar

2. Temperature: 120 °C

MegaWatSoft

Steam Tables

[Excel Add-In](#) [ActiveX DLL](#) [Win32 App](#)

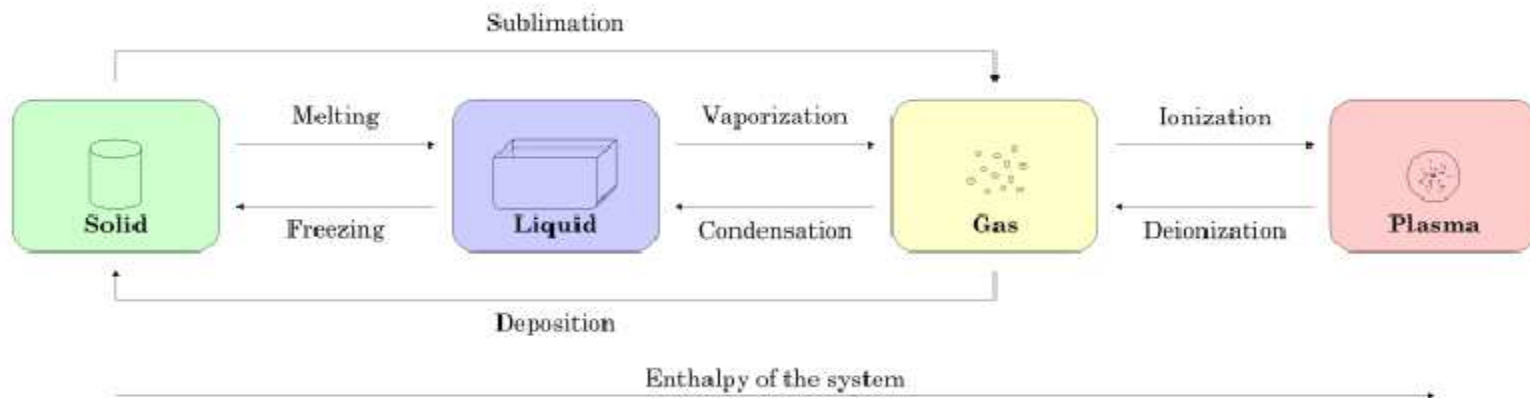
| Property Name | Property ID | Results | Units (SI) | Constants used in calculation |
|--|-------------|-----------------|---------------|--|
| 1. Thermodynamic Properties - Main | | | | |
| 1 Pressure (absolute) | p | 50.0000000000 | bar | Specific gas constant: R = 0.461526 kJ/(kg·K) |
| 2 Temperature | t | 120.0000000000 | °C | Molar gas constant: Rm = 8.31451 J/(mol·K) |
| 3 Density | d | 945.4896942904 | kg/m³ | Molar mass: M = 18.015257 g/mol |
| 4 Specific volume | v | 0.0010576530 | m³/kg | Critical temperature: Tc = 647.096 K, (373.946 °C) |
| 5 Specific enthalpy | h | 507.1654319265 | kJ/kg | Critical pressure: pc = 22.064 MPa, (220.64 bar) |
| 6 Specific entropy | s | 1.5234816447 | kJ/(kg·K) | Critical density: rhoc = 322 kg/m³ |
| 7 Specific exergy | ex | 389.8573452846 | kJ/kg | Triple-point temperature: Tt = 273.16 K, (0.01 °C) |
| 8 Specific internal energy | u | 501.8771669881 | kJ/kg | Triple-point pressure: pt = 611.657 Pa, (0.00611657 bar) |
| 9 Specific isobaric heat capacity | cp | 4.2342873597 | kJ/(kg·K) | |
| 10 Specific isochoric heat capacity | cv | 3.6623197872 | kJ/(kg·K) | |
| 11 Speed of sound | w | 1531.8497680161 | m/s | |
| 2. Thermodynamic Properties - Other | | | | |
| 12 Isentropic exponent | kapa | 443.7303612950 | dimensionless | |
| 13 Specific Helmholtz free energy | H | -97.0796416317 | kJ/kg | |
| 14 Specific Gibbs free energy | G | -91.7913766933 | kJ/kg | |
| 15 Compressibility factor | z | 0.9791446439 | dimensionless | |

Output Pane (* registration required)

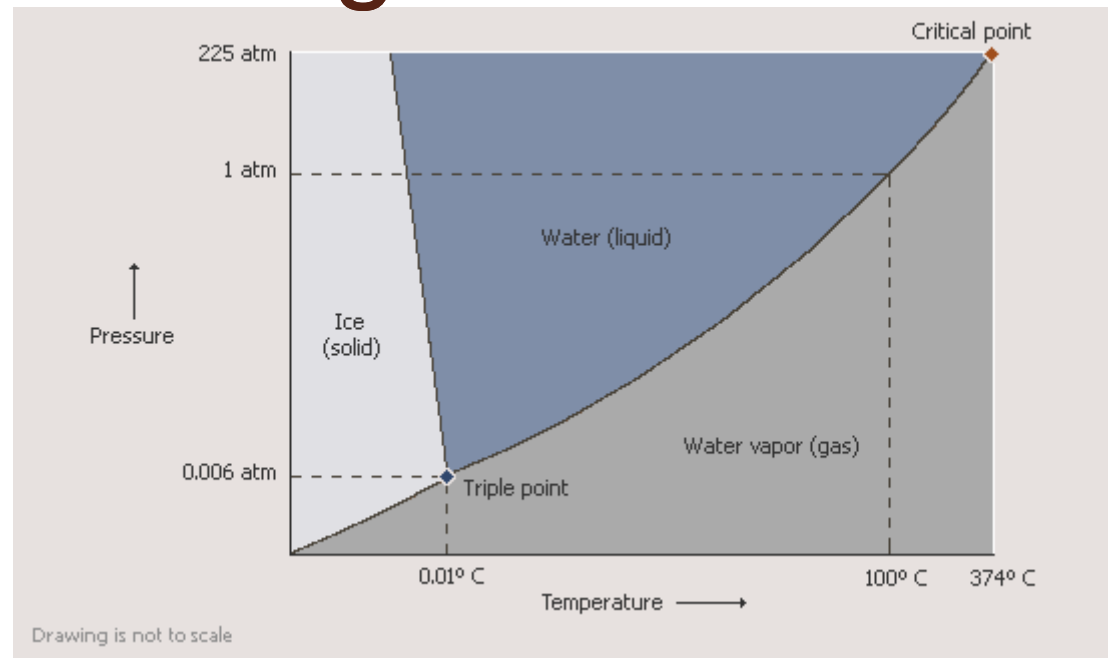
| * | p [bar] | t [°C] | v [m³/kg] | h [kJ/kg] | s [kJ/(kg·K)] | ex [kJ/kg] | u [kJ/kg] | cp [kJ/(kg·K)] | cv [kJ/(kg·K)] | w [m/s] |
|---|---------------|----------------|--------------|----------------|---------------|----------------|----------------|----------------|----------------|-----------------|
| 1 | 50.0000000000 | 120.0000000000 | 0.0010576530 | 507.1654319265 | 1.5234816447 | 389.8573452846 | 501.8771669881 | 4.2342873597 | 3.6623197872 | 1531.8497680161 |
| 2 | | | | | | | | | | |
| 3 | | | | | | | | | | |
| 4 | | | | | | | | | | |
| 5 | | | | | | | | | | |

SI Units | English Units

Phase transitions



Phase diagram of the water



Freezing and melting

- Transferred mass during melting:

$$\Delta M = \frac{\Delta Q}{L_m}$$

- The transferred heat does not change the temperature during the melting
- The melting temperature is depends on the pressure
 - Higher pressure cause lower melting point
 - Experiment with an icecube and a string
- Latent heat (L_m [kJ/kg]):
 - The heat which is absorbed during the melting of 1 kg matter

Boiling and condensation


- Transferred mass in phase transition:

$$\Delta M = \frac{\Delta Q}{L_v}$$

- The temperature does not change during the phase transition
- Why not to try to cook gulasch on Mont Everest?
 - The pressure affects the boiling point
 - Higher pressure cause higher boiling point
- The latent heat disappears approaching the critical point
- Above the critical point the vapour and fluid cannot be distinguished



SZÜNET?



Interactions – not isolated systems

- Mechanical interaction
 - Deformation
 - pressure difference (intensive)
 - Volume change (extensive)
- Electrostatic interaction
 - Different electrostatic potential (int.) cause the flow of the charge (ext.)
- Matter interaction:
 - Mass transition (ext.)
 - Different concentration (chemical potential), (int.)



Equilibrium

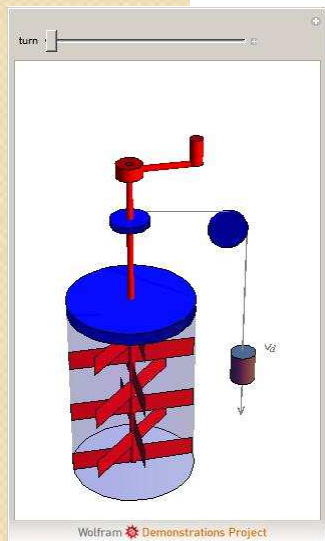
- Processes goes to the equilibrium state (pressure and temperature differences disappears in time)
- Equilibrium necessary condition:
 - Spacial homogeneity of all intensive quantity

System description

- As much number of statevariable as the number of interaction takes place is needed.
- Only extensive variables can be used for the description of the system, but only intensive variable is not enough – minimum one extensive variable is needed (what is the extent/size of the system?)
- Usually more statevariable then interaction => there are algebraic dependencies between them:
 - Stateequations
- Example:
 - Homogeneous system(statevariables: p, V, n, T) - 4
 - Interactions: mechanic, thermic, material – 3
 - $F(p, V, T, n)=0$, ideal gas: $pV = nRT$

Energy exchange between the system & environment

- Experiences:
 - Mechanical work disappears – bouncing ball
 - Warm bodies can exert mechanical work
- Let's do some work on a system – what happens?



Joule's experiment:

- Adiabatic insulated system (fluid)
- Mechanic energy with a mixer
- The temperature increased
- Same ammount of work – same amount of temperature increase
- Electonic work produce the same phenomena

Internal energy

- Adiabatically insulated system in state A
- The **same** amount of work (mechanical, electric, chemical etc...) is needed to bring the system to state B.
- There must be some „property” of the system which change during this interaction!
- Internal energy can be introduced:

$$\Delta U = U_B - U_A = W_{adiabatic}$$

First law of TD

- The internal energy is a *statefunction*:
 - Depends only on the statevariables
 - $U = U(p, V, n)$ $U = U(T, V, n)$ $U = U(p, T, n)$
- Not only work can change the internal energy
 - Contact to body with different temperatures – heat transfer
- *First law of thermodynamics*:
$$dU = \delta Q + \delta W$$
 - U is the internal energy
 - Q is the transferred heat
 - W is the work
- This energy balance equations works in every heat-exchange and in whatever macroscopic work is considered

Internal energy change

$$dU = \delta Q + \delta W$$

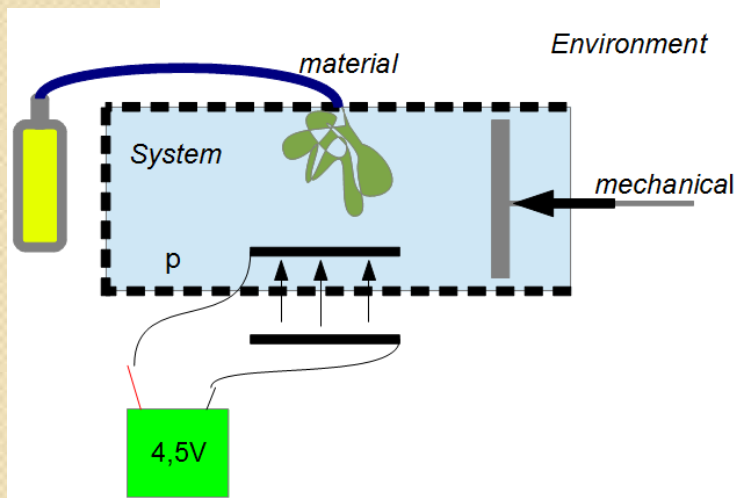
- The equation defines only the change of the internal energy
- Is there a zero point, where $U(x) = 0$?
- The zero point is arbitrary defined:
 - E.g. water, 300 K and 1 atm
- U is determined by the statevariables
- Example: cycle process
 - Internal energy must be the same at the beginning and the end: $\Delta U = 0$
 - Work became heat: $\Delta Q = -\Delta W$

The work in general

- Different kind of work according to the interaction of the system with the environment.
- General form of work:

$$\delta W_i = X_i \cdot d\xi_i$$

- Where X_i is a thermodynamic force
- ξ_i is the extensive quantity



- Mechanical interaction
 - The volume of the system changes

$$\delta W_{mech} = -p \cdot dV$$

- Electrostatic interaction
 - Charges in the system change

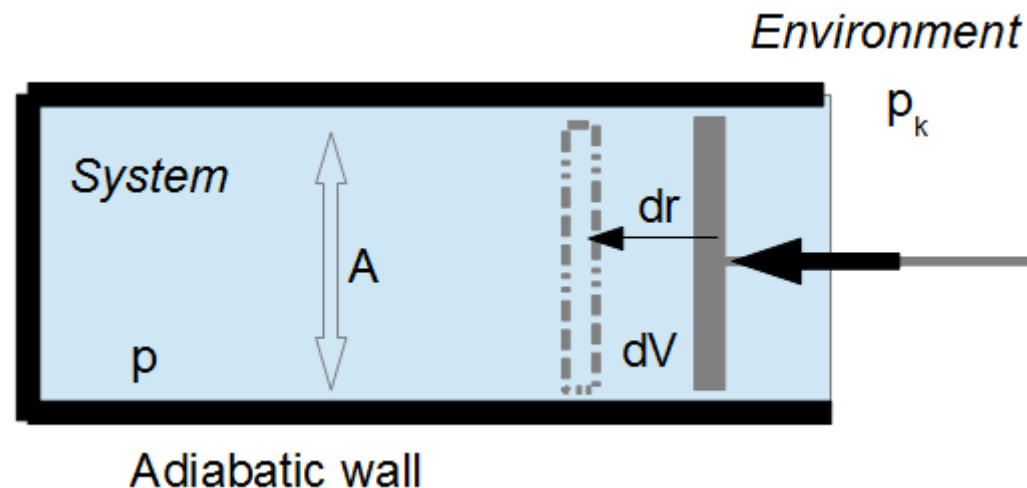
$$\delta W_{el} = \phi \cdot dq$$

- Material interaction
 - The mass change in the system

$$\delta W_{el} = \mu \cdot dn$$

The mechanical work

- *Work (def.):* $dW = \{\text{force}\} \cdot \{\text{displacement}\} = F \cdot dr$
- *Pressure (def.):* $p = \frac{\{\text{force}\}}{\{\text{area}\}} = \frac{F}{A}$
- So the environment work done on this system:
 - $dW = F \cdot dr = (p_k \cdot A)dr = p_k \cdot (Adr) = -p_k dV$



Enthalpy

- TD. I. principle: $dU = \delta Q + \delta W$
- If only mechanical work acts: $\delta W = -p \cdot dV$
- $dU = \delta Q - p dV$
- **Enthalpy definition:**
 - Enthalpy is the inner energy of the system and the energy which is needed to construct a system in its environment
- **Enthalpy change:**

$$dH = dU + d(pV) = dU + dp \cdot V + dV \cdot p = \delta Q - p dV + dp \cdot V + dV \cdot p$$

$$dH = \delta Q + V dp$$

- Advantage in case of open tank: $dp = 0 \Rightarrow dH = \delta Q$
- Specific enthalpy:
 - Intensive quantity
 - Measurement unit: kJ/kg

$$h = \frac{H}{M}$$



Heat transfer

- Forms:
 - Heat radiation (Sun, furnace, flame...)
 - Very complicated
 - Stefan-Boltzmann law
 - Conduction (thermal diffusion)
 - why put a spoon into the hot tee?
 - Temperature inhomogeneity in a material cause heat flow
 - Distributed parameter systems
 - Convective heat transfer:
 - transfer of heat from one place to another by the movement of fluids

Convective heat transfer

- Fourier's law:

$$\frac{dQ}{dt} = \lambda \cdot A \cdot (T_A - T_B)$$

- Q: heat [J];
 - λ : heat transfer coeff. [W/m²/K]
 - A: surface [m²]
 - T: temperature [K]
- Heat transfer coeff. depends on the circumstances:
 - Geometry
 - Temperature of the wall and fluid
 - Pressure
 - Type of convection (laminar flow or turbulent)
- Can be calculated from steady state measured data or semi-empirical formulas

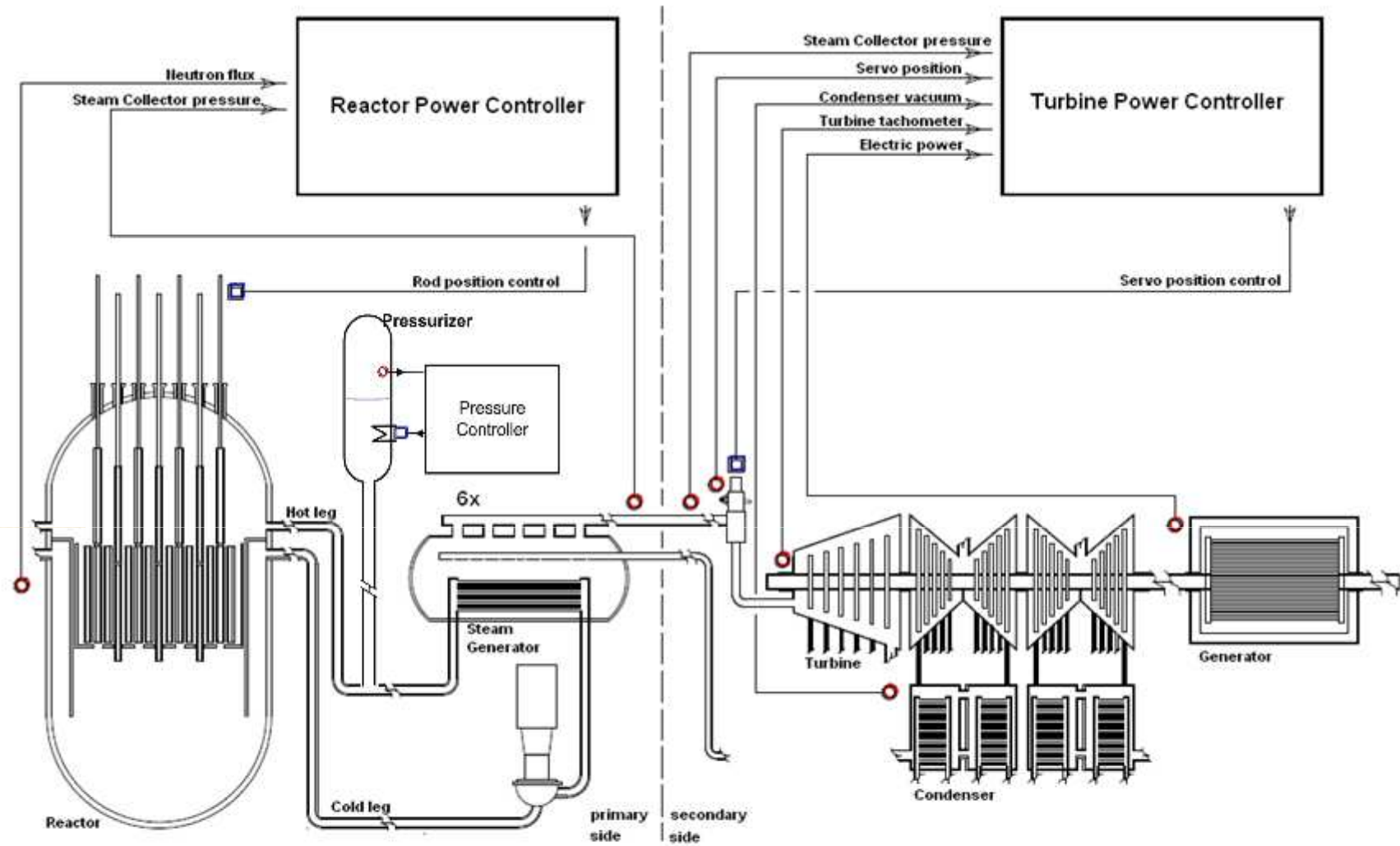
Need a break?



model equations



ENERGY SYSTEMS



Parts of energy systems -

Primary circuit

Aim:

- fresh steam production for the turbines
- Quantity (m) and quality criterions – efficiency

Parts in a nuclear power plant:

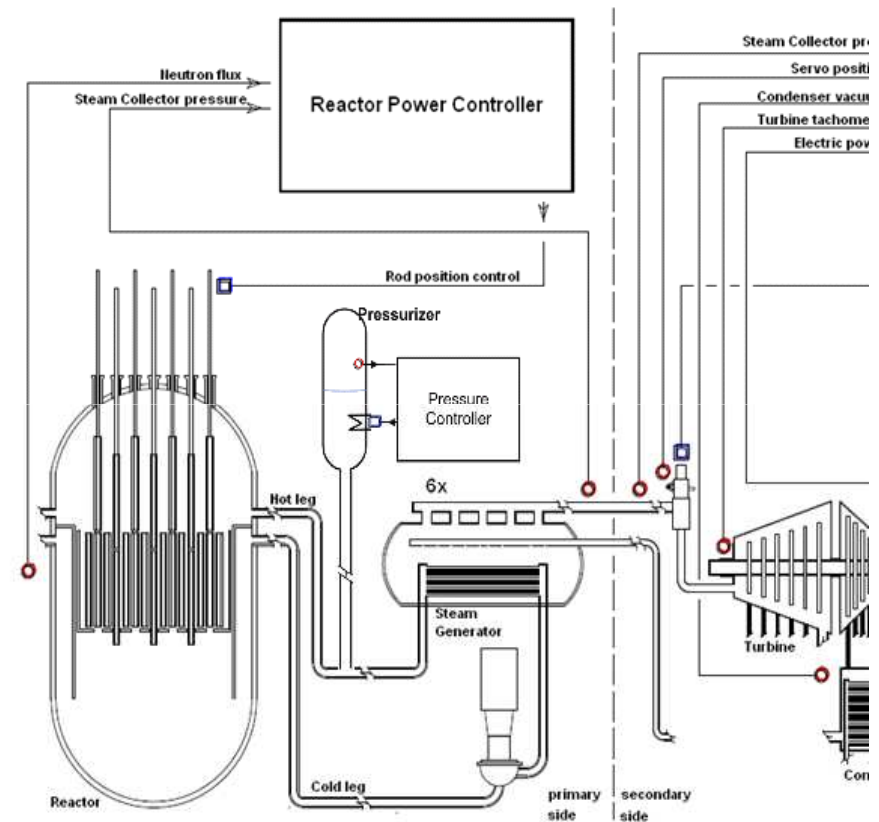
- Reactor vessel, active zone, reactor core
- Hot-leg, and cold-leg (pipes)
- Main coolant pumps
- Steam generators produce steam
- Pressurizer

Parts in a thermal power plant

- Coal hopper, conveyor, pulverizer (tartály, szállítószalag, porlasztó/örlő)
- Furnace
- Boilers generate steam

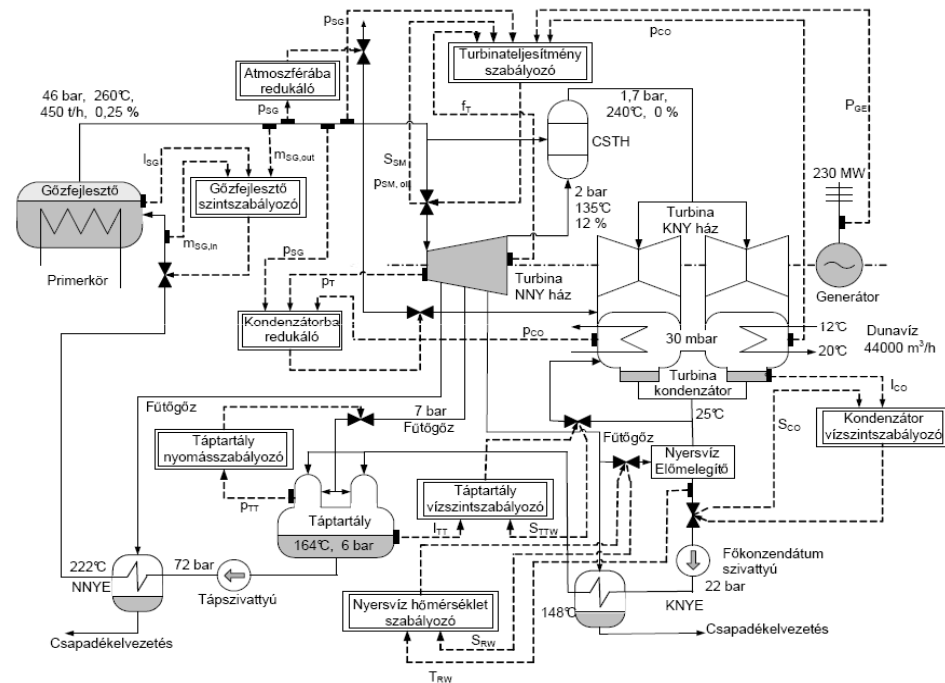
Thermal energy production:

- burning (coal, oil, wood, energy-grass ...) in furnace
 - Chemical reaction: exotherm, $C \rightarrow CO, CO_2$
- Alternative source – nuclear fission in active zone
 - Nuclear reaction, Uranium, Plutonium
- Results:
 - Hot water or air
- Heat transfer and/or radiation




Parts of energy systems 2

- Secondary circuit
 - Aim:
 - Electricity production
 - Parts:
 - Steam control valve
 - Steam turbines (high and low pressure turbines)
 - Super-heaters
 - Condenser
 - Feed water tanks
 - Feed water heaters
 - Water pumps
 - Generators

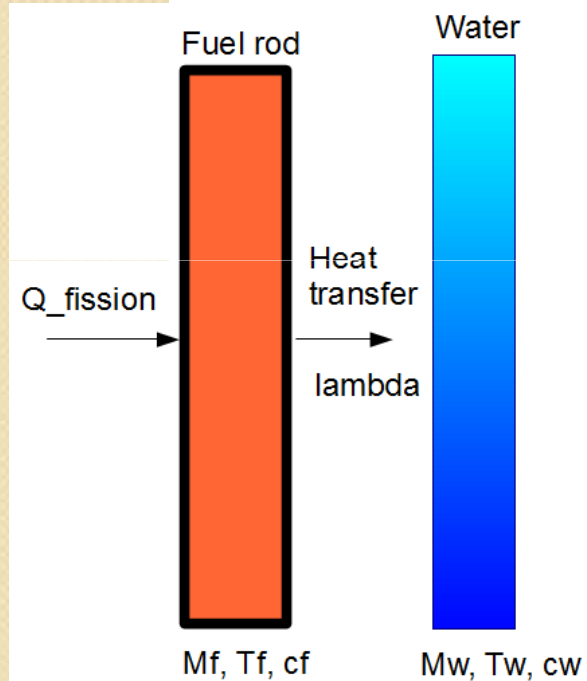


2. ábra. A szekunder kör felépítése.



Lumped parameter Model equations

Fuel rods



- Modeling goal:

- Compute the average temperature of the fuel rods

- Fuel rods:

- 123*350 piece in the reactor core
- UO2 fuel and zirconium clad

- Modeling assumptions:

- Mixed fuel and clad
- All fuel rods is modelled as one rod
- Same temperature
- Homogenous heat generation
- Constant properties (*source of information*):
 - Density (tables)
 - Volume (geometry)
 - Specific heat (tables)
 - Heat transfer parameter (steady state calculation / par. est)
 - Surface (core geometry)

- Main phenomena:

- nuclear fission - heat production given (model input)
- Heat transfer to the coolant, which temperature is known (model input)

$$\frac{dT_f}{dt} = \frac{1}{M_f c_f} (Q_{fission}(t) - A\lambda(T_f - T_w))$$



Simulink model

- Heated_body.mdl:
 - Electrically heated pipe
 - Constant water temperature (80°C) and heat transfer parameter $*A = 200$ W/K
 - Initial condition:
 - 150 °C body temperature
 - No heating power
 - 150 s:
 - Turn on heating (2 kW)
 - Facts:
 - Exponentially decreasing temperature to the equilibrium
 - The system is stable
 - After heating is switched on -> new equilibrium state (exp.)
 - Try:
 - Change the water temperature
 - Change the body mass
 - Change the heat transfer coefficient
 - Compare the results

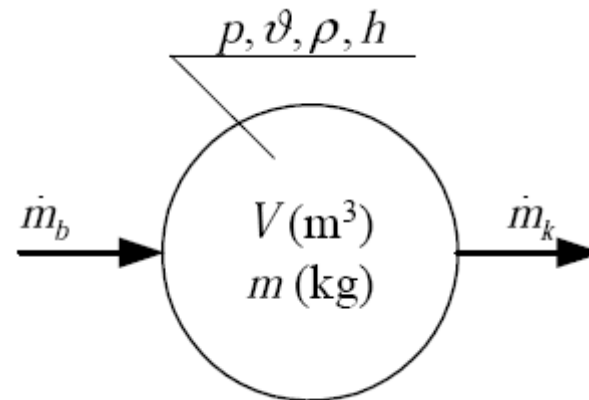


Description of the coolant water

- In solid matter
 - Phenomena:
 - Heat conduction
 - Heat transfer
 - Radiation
 - Heat production
 - No mass transfer → mass balance is not needed
- In liquid matter:
 - Displacement of the matter cause the displacement of its energy aswell
 - Convective heat transport
 - Mass transport

Mass balance equation in generality

- Lumped parameter description
 - Same condition (par.) in the control volume
 - Transport phenomena on the boundary is important
- Notations:
 - \dot{m} mass transfer [kg/s]
 - M mass [kg]
 - V volume [m^3]
 - p pressure [Pa]
 - T (ϑ) temperature [$^{\circ}\text{C}$]
 - ρ density [kg/m^3]
 - h specific enthalpy [J/kg]



Mass balance equation in generality

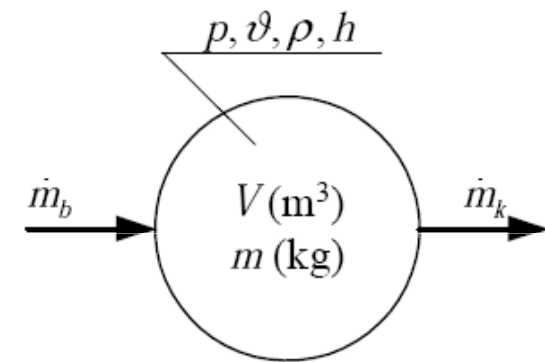
- Mass balance: mass transport through the boundary

$$\frac{dM}{dt} = m_b - m_k$$

- Usually the reformulation of the needed:

$$M = \rho \cdot V$$

$$\frac{dM}{dt} = \frac{d(\rho V)}{dt} = \rho \frac{dV}{dt} + V \frac{d\rho}{dt} = m_b - m_k$$



- Simplification can be used in special cases
 - Is the volume or density constant?
 - 3 cases: volume, density or both can change

1. Density and volume can change

$$\rho \frac{dV}{dt} + V \frac{d\rho}{dt} = m_b - m_k$$

- If the media is *fluid* (water, oil, etc.) we usually want to know its volume-change (*water in furnace's vessel*):

$$\frac{dV}{dt} = \frac{1}{\rho} (m_b - m_k - V \frac{d\rho}{dt})$$

- If the media is *gas or vapour*, we usually want to know its pressure

- Using:
$$d\rho = \frac{\partial \rho}{\partial T} dT + \frac{\partial \rho}{\partial p} dp$$

- After substitution and rearrangement:

$$\frac{dp}{dt} = \frac{1}{V(\partial \rho / \partial p)} \left(m_b - m_k - \rho \frac{dV}{dt} - V \left(\frac{\partial \rho}{\partial T} \right) \frac{dT}{dt} \right)$$

2. The density is constant

$$\rho \frac{dV}{dt} + V \frac{d\rho}{dt} = m_b - m_k$$

$$\rho = \text{const.} \quad d\rho = 0$$

- If the vessel is open, usually we want to know the water level in the tank

$$\rho \frac{dV}{dt} = m_b - m_k$$

- If the crosssection (A) is constant, then the level can be computed as ($V = A * H$):

$$\frac{dH}{dt} = \frac{1}{\rho A} (m_b - m_k)$$

3. The volume is constant

$$\rho \frac{dV}{dt} + V \frac{d\rho}{dt} = m_b - m_k$$

$$V = \text{const.} \quad dV = 0$$

- A fully filled tank, where the density can change.

$$V \frac{d\rho}{dt} = m_b - m_k$$

- If we interested in pressure:

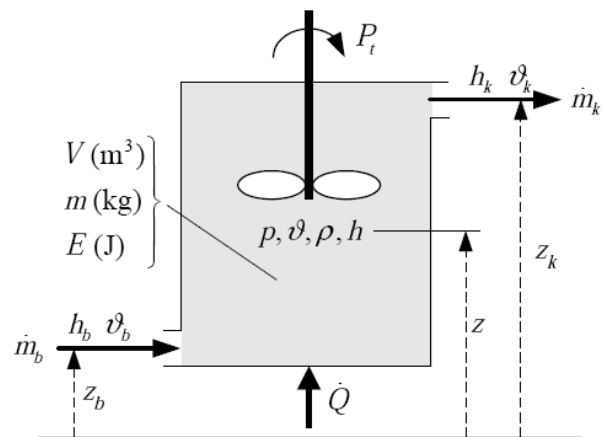
$$d\rho = \frac{\partial \rho}{\partial T} dT + \frac{\partial \rho}{\partial p} dp$$

- using the relationship:

$$\frac{dp}{dt} = \frac{1}{V(\partial \rho / \partial p)} \left(m_b - m_k - V \left(\frac{\partial \rho}{\partial T} \right) \frac{dT}{dt} \right)$$

Energy Balance Equation

- Control volume - boundary of the system
- TD. II. principle:
 - Heat transfer
 - Mass transfer
 - work on environment

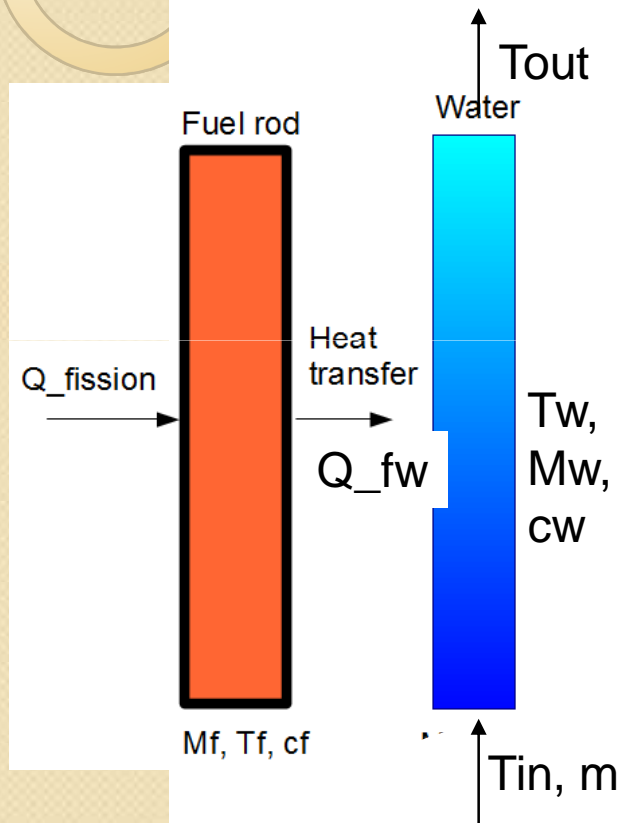


2-15. ábra.

A koncentrált energiátárolás jellemzői

$$\underbrace{\frac{d}{dt}(E)}_{\text{A tárolt energia megváltozása}} = \underbrace{(\dot{m}_b e_b - \dot{m}_k e_k)}_{\text{Be- és kivitt konvektív energiaáram}} + \underbrace{\dot{Q}}_{\text{Kívülről bevezetett hőteljesítmény}} - \underbrace{\dot{W}_t}_{\text{Környezeten végzett mech. munka}}$$

Coolant modeling



- Modeling goal:
 - Coolant average temperature
 - Coolant outlet temperature
- Assumptions:
 - Model inputs:
 - heating power from the fuel rod (Q_{fw})
 - inlet water temperature (T_{in})
 - Model output:
 - Water average temperature (T_w)
 - Outlet temperature (T_{out})
 - Constant properties:
 - Specific heat capacity (steamtable)
 - Volume (geometry)
 - density (steamtable)

Energy balance equation for a heated pipe

$$\frac{dE}{dt} = m_b h_b - m_k h_k + Q$$

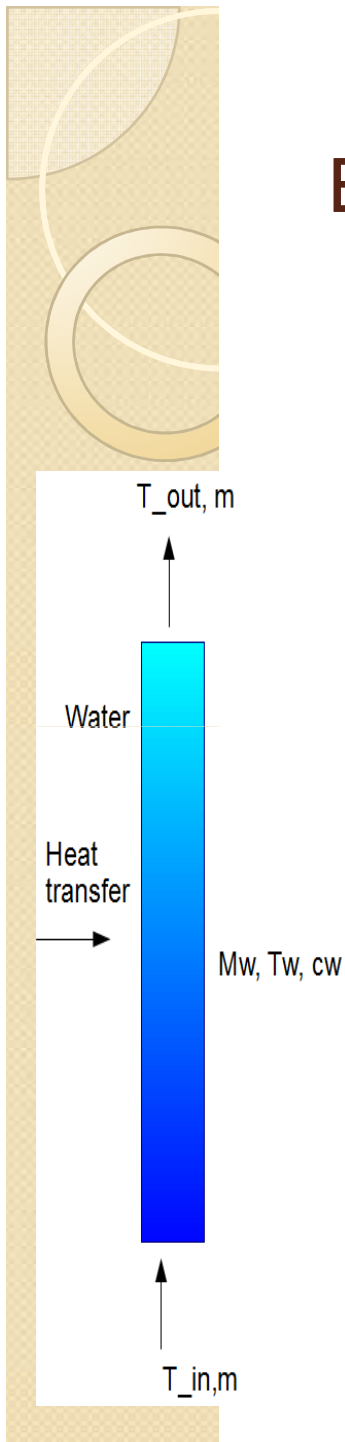
- If there is no phase-change, using the temperature is more convenient
 - Linear relationship between the temperature and enthalpy: $h = cT$
- Rewriting the left side: $\frac{dE}{dt} = \frac{d(cMT)}{dt} = cM \frac{dT}{dt} + cT \frac{dM}{dt}$

- The mass balance is needed:

$$\frac{dM}{dt} = m_b - m_k$$

- Finally: $\frac{dT}{dt} = \frac{1}{Mc} (m_b c(T_b - T) - m_k c(T_k - T) + Q)$

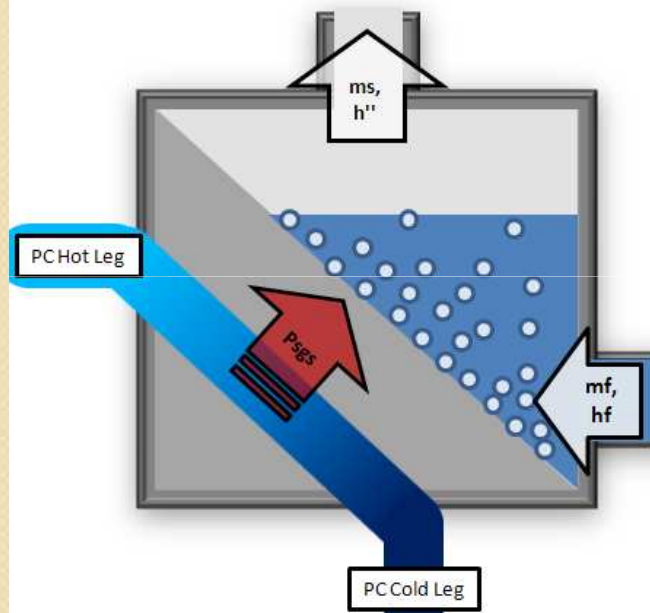
- What is T_k ?
 - $T_{ave} = (T_b + T_k)/2$ Not correct during dynamics, why?
 - $cm(T_k - T_{ave}) = cm(T_k - T_b)/2 = Q/2$ or
 - Delayed: $T_{ki}(t) = T_b(t-T) + T_{ave}(t-T/2)$



Pipe modell

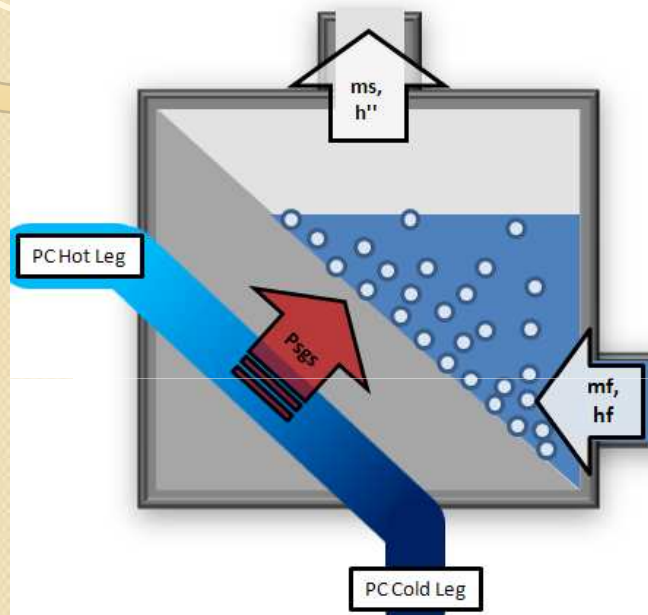
- Matlab Simulink
 - heated_pipe.mdl
- Initial condition:
 - No heating
- Steady state: what flows in that flows out
- 150s heating turned on:
 - New equilibrium point
 - In new steadytate: $dT_{ave} = dT_{out}/2$
- Try:
 - Mass transfer changes
 - Change the volume of the pipe
 - Inlet temperature changes
 - Compare the results

Steam generator secondary side model



- Steam generator
 - Ca. 5500 heated pipe
- Primary side
 - cooled pipe
- *Secondary side*
 - saturated water and steam
- Modelling goal:
 - Compute the pressure on the SC
 - Compute the temperature on the SC
- Assumptions:
 - Saturated water and steam in one control volume
 - $V = V_w + V_s$ mass of water and steam
 - Model inputs:
 - Feed water enthalpy and mass flow
 - Fresh steam mass flow
 - Heating power from the PC
 - Model outputs:
 - Pressure, temperature

Steam generator model



- Mass and energy balance equations:

$$\frac{dM}{dt} = m_f - m_s$$

$$\frac{dU}{dt} = P_{sgs}/6 + m_f h_f - m_s h''$$

- Mass to water volume:

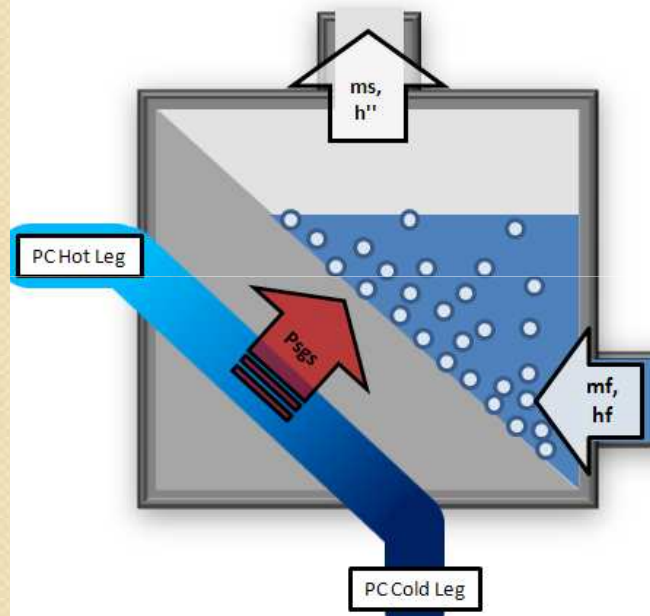
$$\frac{dV_w}{dt} = \frac{1}{\rho_w - \rho_s} \left(m_f - m_s - \left(V_s \frac{d\rho_s}{dp} + V_w \frac{d\rho_w}{dp} \right) \frac{dp_{sg}}{dt} \right)$$

- The volume depends on the pressure because the density depends on the pressure

- Pressure from energy balance:

$$\frac{dp_{sg}}{dt} = \frac{\left(1 - \frac{\rho_s}{\rho_w}\right) \frac{P_{sgs}}{h'' - h'} + m_f \left(\frac{\rho_s}{\rho_w} \frac{h'' - h_f}{h'' - h'} - \frac{h' - h_f}{h'' - h'} \right) - m_s}{V_w a(p_{sg}) + (V - V_w) b(p_{sg})}$$

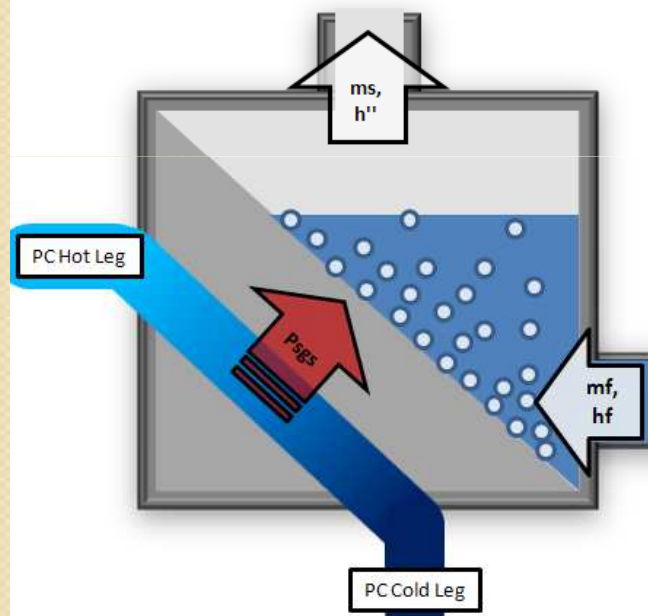
Steam generator Simulink modell 1



- steamGenerator.mdl
- initSteadyState.m
- Initial condition
 - Constant heating (1375MW/6)
 - Constant mass flow (123 kg/s)
- Facts:
 - Non-stable model output
 - Not feedback to the heat transfer!

Steam generator Simulink modell 2

- Steam generator modell + primary circuit pipe
- Not the transferred heat, but the primary side temperature is the model input
 - Higher pressure -> higher SC temperature -> smaller temp. Difference → smaller heat transfer, which stabilize the system!



Steam collector modell

- Steam collector connects the steam generator to the turbine
- Modeling goal:
 - Compute the pressure in the collector
- Model inputs:
 - Turbine steam consumption (m_{tu})
 - Mass flow into the collector (m_s)
- Model output:
 - Steam collector pressure
- Modeling assumptions:
 - Constant temperature (no need of Energy balance equation)
 - Only steam in the collector
 - Steam density depends only on the pressure

- Mass balance equation:

$$\frac{dM_c}{dt} = m_{sg} - m_{tu}$$

- Mass balance to pressure:

$$\frac{dp_c}{dt} = \frac{m_{sg} - m_{tu}}{\frac{d\rho_c}{dp_c} V_c}$$

Steam collector Simulink Model

- Collector.mdl
- Initial condition
 - $m_{in} = m_{out} = 123 \text{ kg/s}$
- Step function in m_{in} ($123 \rightarrow 120 \text{ kg/s}$)
 - Pressure constantly decreasing
 - Non-stable...
 - Solution:
 - mass transfer depends on the pressure!
 - Bernoulli's law