# Dynamic system modeling for control and diagnosis Modelling of mechanical systems

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## Mechanical systems - 1

Characterization: through mechanisms and modeling objects

**Modeling objects**: called "bodies" for which conservation balances are constructed

- elementary object: *mass point*
- models of "mass point systems" result in concentrated parameter models
- rigid bodies
- deformable bodies

Mechanisms: for which constitutive equations are available

- forces originating from a potential field, e.g. *spring*
- gravitation
- friction
- torsion, deformation (elastic, non-elastic), etc.

## Mechanical systems - 2

**Basic principles**: Newton - Principia Mathematica Phylosophiae Naturalis (1687)

- 1. Each object (body) keeps its steady-state position or its rectilinear motion with constant velocity unless an external effect forces it to change.
  - equivalent coordinate systems move with constant relative velocity
  - external effects described by forces
- 2. The change of *momentum* is proportional to the effect of the force and takes place in the direction of the force.
  - both the momentum and the force are vectors, thus they have magnitude and direction
  - *momentum is a conserved extensive quantity*
- 3. The effect is equal to the reaction, that is, the effect of two bodies to each other is of equal magnitude but of adverse direction.

Rectilinear motions

## Modeling of mechanical systems - 1

### I. Rectilinear motions

simplest case: mass-point systems

**Conservation balances**: momentum balance in each considered direction for each mass point

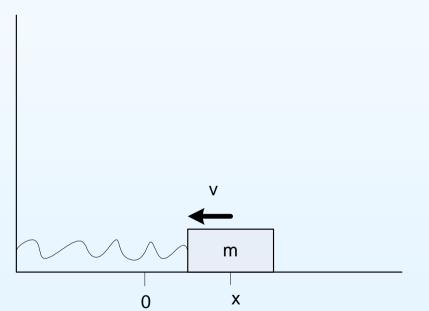
### **Constitutive equations**

- static equation(s) for each force from the physics of its underlying mechanism
  - $^{\circ}$  gravitation:  $F_g = m \cdot g$
  - $\circ$  friction:  $F_f = \mu \cdot m \cdot g$
  - $\circ$  elastic force (e.g. in spring):  $F_s = -k \cdot x$  position dependent!
  - other position dependent forces (e.g. from a potential, electrical forces)
- *dynamic position-momentum equation* (if needed)

## Example: mass and spring

### **Problem description**

Given a mass point *m* connected to the wall by an elastic spring with spring coefficient *k* and moving along a horizontal line. The mass is under the influence of an external force  $F_e$  and there is a friction with a coefficient  $\mu$ .



Construct the model of the mass-spring system for control purposes if we can measure the position of the mass point x and the external force  $F_e$ .

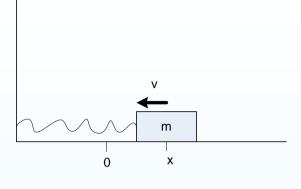
## Example: mass and spring - 2

### Mechanisms

- spring
- friction generated by the gravitational force
- external force  $F_e$

### **Modeling assumptions**

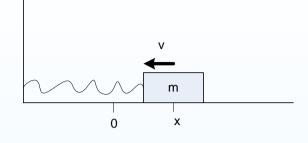
- F1 one mass point with mass m
- F2 rectilinear motion
- F3 elastic ideal spring with coefficient k (force  $F_s$ )
- F4 friction with constant coefficient  $\mu$  (force  $F_f$ )
- F5 position origo x = 0 is at the equilibrium point



Example: mass and spring - 3

**Conservation balance equation:** 

for momentum  $p = m \cdot v$ 



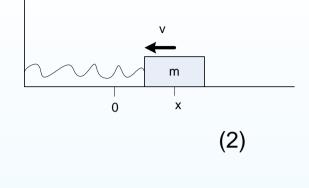
$$\frac{dp}{dt} = F_f + F_s + F_e \tag{1}$$

### **Constitutive equations**

- $F_f = \mu \cdot m \cdot g$  (friction)
- $F_s = -k \cdot x$  (spring)
- $p = m \cdot v = m \cdot \frac{dx}{dt}$  (position is measurable)

### Example: mass and spring - 4

### Model equations with measurable variables:



### **State-space model form**

• state variables: position x and momentum (p, or v)

 $\frac{dx}{dt} = \frac{1}{m}p$ 

 $\frac{dp}{dt} = \mu \cdot m \cdot g - k \cdot x + F_e$ 

- input variable: external force  $F_e$
- output variable: position x

(3)



## Rotating motions

Dynamic modelling - 5. - p. 11/2

## Modeling of mechanical systems - 2



II. Rotating motions

simplest case: mass-point systems

Characteristic variables and parameters

- angular momentum N (analogue to the momentum p)
- angle velocity (angular frequency)  $\omega$  ( $[\frac{rad}{s}]$ )
- moment of inertia  $\Theta$  (for mass point  $m_i$ :  $\Theta_i = m_i \cdot r_i^2$
- torque  $M = F \times r$  in [Nm] r is the distance from the rotating axis

**Conservation balances**: angular momentum balance in each considered direction for each rotating mass point

$$\frac{dN}{dt} = \sum_{k} M_k \tag{4}$$

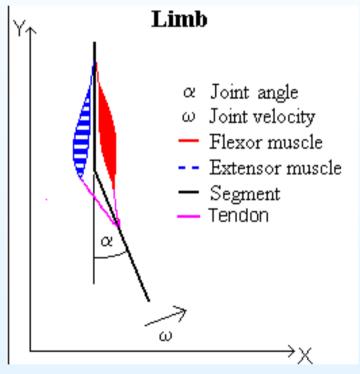
with the external torques  $M_k$ 

Example: a simple limb model - 1



### **Problem description**

Given a simple limb consisting of two segments (bones) two muscles (flexor and extensor) that move the lower segment around the joint axis.



Construct the model of the simple limb system for control purposes if we can measure the position of lower segment and the external forces causing contraction on the flexor and extensor muscles, respectively.

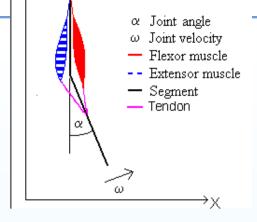
## Example: a simple limb model - 2

### Mechanisms

- muscle force
- muscle contraction by activation
- rotation

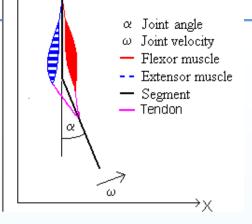
## **Modeling assumptions**

- F1 one mass point with mass m for the lower segment
- F2 the upper segment is fixed vertically
- F3 fixed distance  $l_{COM}$  from the rotating axis
- F4 activation state equations with fixed parameters ( $\tau$  activation time,  $\beta$  descreasing factor)
- F5 activation determines the torque of the muscles  ${\cal M}$



Example: a simple limb model - 3

Conservation balance equations: for angular momentum  $N = \Theta^{(total)} \cdot \omega$ 



$$\frac{dN}{dt} = M(q_1, q_2, \alpha, \omega) + m \cdot l_{COM} \cdot \cos(\alpha - \frac{\pi}{2}) \cdot g$$
(5)

for the acticvation states  $q_1$  and  $q_2$  (bioelectrical model)

$$\frac{dq_1}{dt} = \left(\frac{1}{\tau_{act}}(\beta + [1 - \beta]u^f(t))\right)q_1 + \frac{1}{\tau_{act}}u^f(t) \quad (6)$$

$$\frac{dq_2}{dt} = \left(\frac{1}{\tau_{act}}(\beta + [1 - \beta]u^e(t))\right)q_2 + \frac{1}{\tau_{act}}u^e(t) \quad (7)$$

#### **Constitutive equations**

- $\frac{d\alpha}{dt} = \omega$  (velocity equation)
- the actual form of  $M(q_1, q_2, \alpha, \omega)$  (from biology)



## Thermo-mechanical systems

Modeling of mechanical systems - 3



**III. Energy-based description** – simplest case: mass-point systems

**Rectilinear motion**: potential (position dependent) and kinetic (momentum dependent) energy - for a single mass point with mass m

$$E_{total} = V(x) + \frac{1}{2m}p^2$$

Power  $(\frac{dE_{total}}{dt})$  provided by a force F:  $\frac{dE_{total}}{dt} = F \cdot \frac{dx}{dt} = F \cdot v$ 

**Rotating motion**: kinetic energy for a rotating body with moment of inertia  $\Theta$ 

$$E_{rot} = \frac{1}{2} \Theta \omega^2$$

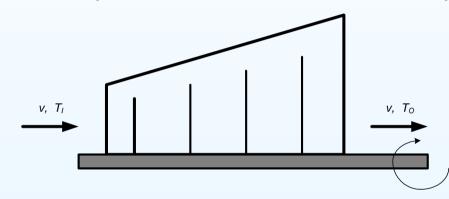
Power  $(\frac{dE_{rot}}{dt})$  provided by a torque M:  $\frac{dE_{rot}}{dt} = M \cdot \omega$ Equivalence with the momentum-based description

## Example: simple steam turbine - 1



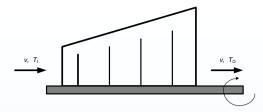
### **Problem description**

Given a simple steam turbine that moves a rotating shaft aroung a given axis. The steam enters and leaves the turbine with a given mass flow rate v, the inlet temperature is  $T_I$ , the outlet temperature is  $T_O$ .



Construct the model of the simple turbine for control purposes if we can measure the external load torque  $M_{load}$  and the angular velocity  $\omega$ .

## Example: simple steam turbine - 2



### Mechanisms

- thermal energy conversion
- rotation

### **Modeling assumptions**

- F1 one rotating body (shaft) with moment of inertia  $\Theta$
- F2 equal and given mass flow rate v for inlet and outlet
- F3 given inlet  $T_I$  and outlet  $T_O$  temperatures (no condensation!)
- F4 the mechanical efficiency factor  $\chi$  is given and constant
- F5 constant steam specific heat  $c_P$
- F6 given the external load torque  $M_{load}$  (input)

Example: simple steam turbine - 3

**Conservation balance equation:** 

for the rotation energy

$$\frac{dE_{rot}}{dt} = P_{steam} - M_{load}\omega \tag{8}$$

### **Constitutive equations**

- $E_{rot} = \frac{1}{2} \Theta \omega^2$  (rotation energy)
- $P_{steam} = \chi \cdot c_P \cdot v \cdot (T_I T_O)$  (power generated by the steam temperature drop)

Model equation with measurable quantities

$$\frac{d\omega}{dt} = \frac{1}{\Theta\omega} \left( \chi \cdot c_P \cdot v \cdot (T_I - T_O) - M_{load} \omega \right)$$

